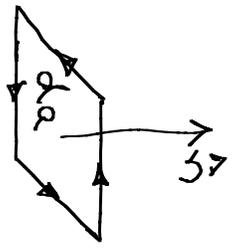


Phys 366

Lecture 9

Vector fields and the curl

Vector field  $\vec{F}$  (circulation of  $\vec{F}$  around closed curve  $C$ ) =  $\oint_C \vec{F} \cdot d\vec{r}$



$\text{curl } \vec{F} \cdot \hat{n} da = \nabla \times \vec{F} \cdot \hat{n} da = \int_C \vec{F} \cdot d\vec{r}$  right-hand rule

Shape of area?

$\nabla \times \vec{F} \cdot \hat{n}$  is the differential version of circulation

Z-component:  $da = dx dy$   
 $\hat{n} = \hat{x} \times \hat{y} = \hat{z}$

Components

Cartesian:  $\nabla \times \vec{F} \cdot \hat{z} da = \underbrace{F_y (x + \frac{1}{2} dx) dy - F_x (x - \frac{1}{2} dx) dy}$

$\frac{\partial F_y}{\partial x} dx dy$

$- F_x (y + \frac{1}{2} dy) dx + F_x (y - \frac{1}{2} dy) dx$

$-\frac{\partial F_x}{\partial y} dy dx$

$$= \left( \frac{\partial F_z}{\partial x} - \frac{\partial F_x}{\partial y} \right) da$$

$$\nabla \times \vec{F} \cdot \hat{z} = \frac{\partial F_z}{\partial x} - \frac{\partial F_x}{\partial y}$$

So we have ( $\nabla$  operator)

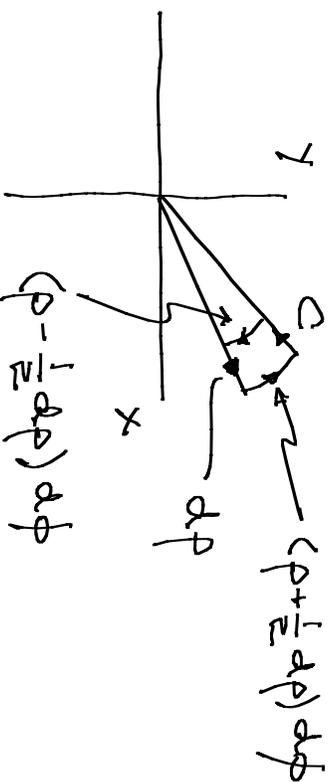
$$\nabla \times \vec{F} = \hat{z} \epsilon_{ijk} \nabla_j F_k = \hat{x} \left( \frac{\partial F_z}{\partial y} - \frac{\partial F_y}{\partial z} \right) + \hat{y} \left( \frac{\partial F_x}{\partial z} - \frac{\partial F_z}{\partial x} \right) + \hat{z} \left( \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right)$$

$\nabla_j \rightarrow \frac{\partial}{\partial x_j}$

$\nabla \times \vec{F}$  is a pseudovector because  $\nabla$  transforms like a vector.

Cylindrical:

$$\nabla \times \vec{F} \cdot \hat{z} = \oint_C \vec{F} \cdot d\vec{x}$$



$$\begin{aligned} &= \underbrace{F_y(\phi - \frac{1}{2} dp) dp - F_y(\phi + \frac{1}{2} dp) dp}_{-\frac{\partial F_y}{\partial x} dp dp} - \underbrace{\frac{\partial F_z}{\partial y} dp dp}_{-\frac{\partial F_z}{\partial y} dp dp} \\ &+ \underbrace{F_x(\rho + \frac{1}{2} dp)(\rho + \frac{1}{2} dp) d\phi - F_x(\rho - \frac{1}{2} dp)(\rho - \frac{1}{2} dp) d\phi}_{\frac{\partial (F_x \rho)}{\partial \rho} dp dp} = \frac{1}{\rho} \frac{\partial (F_x \rho)}{\partial \rho} \rho dp dp \end{aligned}$$

This already shows the two effects. Given a component of  $\nabla \times \vec{F}$  and a coordinate for a derivative, we have to worry about (i) change in the line element for the third coordinate from the front to the back of C and (ii) converting the derivative coordinate to length. So we get

Cylindrical:  $\nabla \times \vec{F} = \hat{\rho} \left( \frac{1}{\rho} \frac{\partial F_z}{\partial \phi} - \frac{\partial F_\phi}{\partial z} \right) + \hat{\phi} \left( \frac{\partial F_\rho}{\partial z} - \frac{\partial F_z}{\partial \rho} \right) + \hat{z} \left( \frac{1}{\rho} \frac{\partial (\rho F_\phi)}{\partial \rho} - \frac{\partial F_\rho}{\partial \phi} \right)$

$\frac{d\rho}{dz}$   $\frac{d\phi}{dz}$   $\frac{dz}{d\rho}$   $\frac{d\rho}{d\phi}$   $\frac{d\rho}{d\phi}$

General:  $\nabla \times \vec{F} = \hat{x}_1 \left( \frac{1}{h_2 h_3} \frac{\partial (h_3 F_3)}{\partial x_2} - \frac{1}{h_2 h_3} \frac{\partial (h_2 F_2)}{\partial x_3} \right)$

length for 3rd coordinate  
length for derivative coordinate

$+ \hat{x}_2 \left( \frac{1}{h_1 h_3} \frac{\partial (h_1 F_1)}{\partial x_3} - \frac{1}{h_1 h_3} \frac{\partial (h_3 F_3)}{\partial x_1} \right)$

$\frac{h_1 dx_1}{h_3 dx_3}$   $\frac{h_3 dx_3}{h_1 dx_1}$

$+ \hat{x}_3 \left( \frac{1}{h_1 h_2} \frac{\partial (h_1 F_1)}{\partial x_1} - \frac{1}{h_1 h_2} \frac{\partial (h_2 F_2)}{\partial x_2} \right)$

$\frac{h_2 dx_2}{h_1 dx_1}$   $\frac{h_1 dx_1}{h_2 dx_2}$

$$\frac{\partial B}{\partial t} \nabla \times \vec{F} = \sum_{i,j,k} \epsilon_{ijk} \frac{1}{h_i h_j h_k} \left( \frac{\partial (h_x F_x)}{\partial x_x} - \frac{\partial (h_x F_x)}{\partial x_x} \right)$$

Spherical:  $\nabla \times \vec{F} = r \left( \frac{1}{r \sin \theta} \frac{\partial (\sin \theta F_\phi)}{\partial \theta} - \frac{1}{\sin \theta} \frac{\partial F_\theta}{\partial \phi} \right) + \theta \left( \frac{1}{r \sin \theta} \frac{\partial F_r}{\partial \phi} - \frac{1}{r} \frac{\partial (r F_\theta)}{\partial r} \right)$

$r \sin \theta d\phi$        $r d\theta$        $r \sin \theta d\phi$   
 $r d\theta$        $r d\theta$        $r d\theta$

$+ \phi \left( \frac{1}{r} \frac{\partial (r F_\theta)}{\partial r} - \frac{1}{r} \frac{\partial F_r}{\partial \theta} \right)$   
 $r d\theta$        $dr$        $r d\theta$

Stokes's theorem:  $\int_S \nabla \times \vec{F} \cdot d\vec{a} = \oint_C \vec{F} \cdot d\vec{s}$

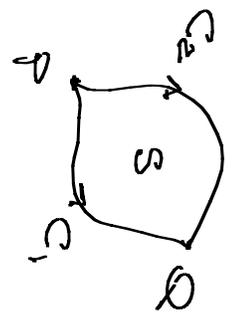
↑  
right-hand rule

Boundary of a boundary is zero:

①  $\nabla \times \nabla f = \hat{e}_j \epsilon_{jka} (\nabla f)_{a,k} = \hat{e}_j \epsilon_{jka} f_{,ka} = 0$

↔  $\int_S \nabla \times \nabla f \cdot d\vec{a} = \oint_C \nabla f \cdot d\vec{s} = 0$

a closed curve has no endpoints



$$\int_{C_1} \nabla f \cdot d\vec{r} - \oint_{C_1} \nabla f \cdot d\vec{r} = \oint_S \nabla \times \nabla f \cdot d\vec{a} = 0$$

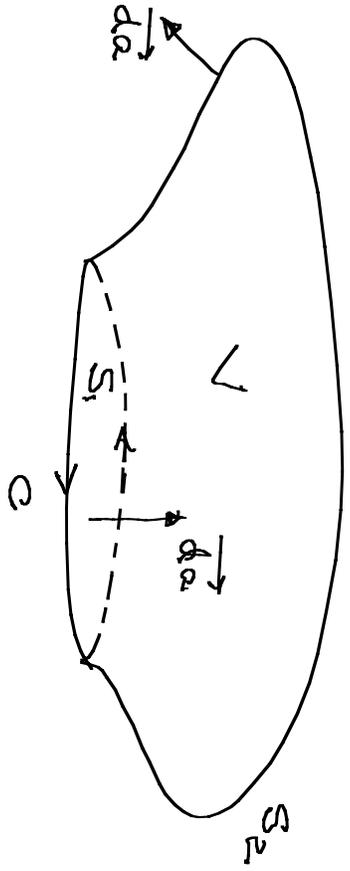
$$= f(Q) - f(P)$$

(2)

$$\nabla \cdot \nabla \times \vec{F} = (\nabla \times \vec{F})_{jij} = \epsilon_{jik} F_{a,ki} = 0$$

$$\Leftrightarrow \int_V \nabla \cdot \nabla \times \vec{F} = \oint_S \nabla \times \vec{F} \cdot d\vec{a} = 0$$

↳ a closed surface has no bounding curve



$$\int_{S_2} \nabla \times \vec{F} \cdot d\vec{a} - \int_{S_1} \nabla \times \vec{F} \cdot d\vec{a} = \int_V \nabla \cdot \nabla \times \vec{F} dV = 0$$

$$= \int_C \vec{F} \cdot d\vec{r}$$

Example:  $\vec{F} = F(r)\hat{\phi}$ ,  $\nabla \times \vec{F} = \hat{r} \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta F(r)) - \hat{\theta} \frac{1}{r} \frac{\partial}{\partial r} (r F(r))$

$= \hat{r} \frac{\cos \theta F(r)}{\sin \theta} - \hat{\theta} \frac{1}{r} \frac{d}{dr} (r F(r))$

$\oint_C \vec{F} \cdot d\vec{l} = \int_0^{2\pi} d\phi \int_0^a r F(r) = 2\pi a F(a)$

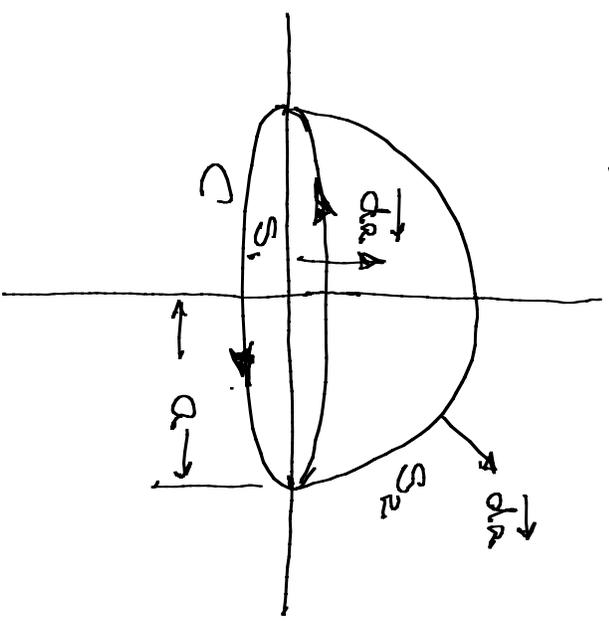
$a d\phi \hat{\phi}$

$\int_{S_1} \nabla \times \vec{F} \cdot d\vec{a} = \int_0^a dr \frac{d}{dr} (r F(r)) \int_0^{2\pi} d\phi = 2\pi a F(a)$

$-\hat{\theta} dr r d\phi$

$\int_{S_2} \nabla \times \vec{F} \cdot d\vec{a} = a F(a) \int_0^{2\pi} d\phi \int_0^{2\pi} d\theta \sin \theta = 2\pi a F(a)$

$\hat{r} a^2 \sin \theta d\theta d\phi$

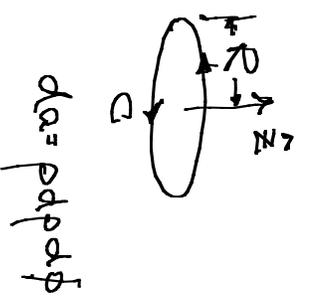


Fluid flow: Let  $\vec{v} = v\hat{z}$ ,  $\vec{v} = v_x \hat{x} + v_y \hat{y} + v_z \hat{z} = v r \sin \theta \hat{\phi} = v r \hat{\phi}$ ,  $\nabla \times \vec{v} = 2v\omega \hat{z}$

$\int_S \nabla \times \vec{v} \cdot \hat{z} da = \oint_C \vec{v} \cdot d\vec{l} = \int_0^{2\pi} v \phi R d\phi = 2\pi v R^2$

$\int_S \nabla \times \vec{v} \cdot d\vec{a} = \frac{2\pi v R^2}{\pi R^2} = 2v$

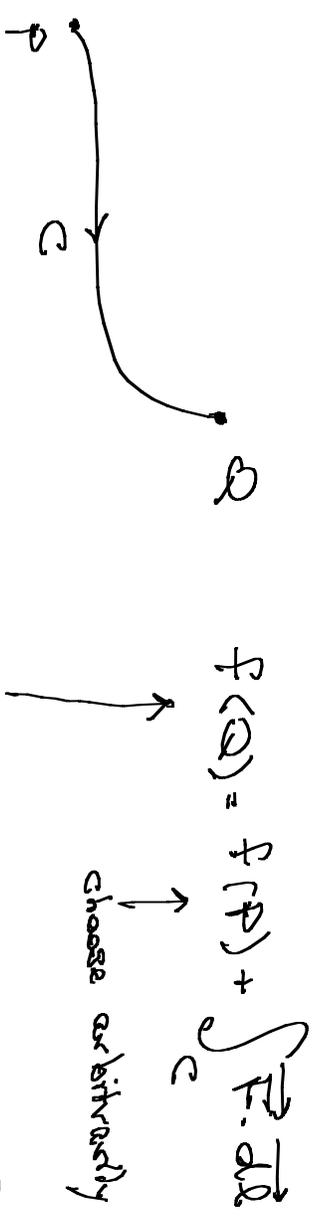
Notice: the vortex line extends to infinity in both directions, even when it's not a straight line.



$da = R d\phi d\phi$

This kind of flow, in which the fluid rotates about a line, is called a vortex. Generally,  $\nabla \times \vec{v}$  is called the vorticity of the flow. Flow without rotation is conservative, i.e.,  $\nabla \times \vec{v} = 0$ .

A conservative field is one that satisfies  $\nabla \times \vec{F} = 0$ . This implies that  $\vec{F} = \nabla f$  for some scalar field  $f$ . You construct  $f$  as follows



$$\nabla \cdot \vec{F} = \nabla \cdot \nabla f = \nabla^2 f$$

$\nabla^2 = \nabla \cdot \nabla$  is called the Laplacian. It arises frequently, since it is the natural second derivative of a scalar field.

Vector differential identities:

$$\nabla(fg) = g\nabla f + f\nabla g \qquad \nabla(\vec{F} \cdot \vec{G}) ?$$

$$\nabla \cdot (f\vec{F}) = \nabla f \cdot \vec{F} + f\nabla \cdot \vec{F}$$

$$\nabla \cdot (\vec{F} \times \vec{G}) = \frac{\partial}{\partial x^i} (\epsilon_{ijk} F_k G_j)$$

$$= \epsilon_{jkl} F_{k;j} G_l + \epsilon_{jkl} F_k G_{l;j}$$

$$= G_l \epsilon_{ajk} F_{k;j} - F_k \epsilon_{kij} G_{l;j}$$

$$= \vec{G} \cdot \nabla \times \vec{F} - \vec{F} \cdot \nabla \times \vec{G}$$

$$\nabla \times (f\vec{F}) = \nabla f \times \vec{F} + f\nabla \times \vec{F}$$

Now for two hard ones:

$$\textcircled{1} \nabla \times (\vec{F} \times \vec{G}) = \hat{e}_j \epsilon_{jkl} (\vec{F} \times \vec{G})_{kl}$$

$$(\epsilon_{jmn} F_m G_n)_{;k} = \epsilon_{jmn} (F_{m;k} G_n + F_m G_{n;k})$$

$$= \hat{e}_j \underbrace{\epsilon_{jkl} \epsilon_{lmn}}_{\delta_{jm} \delta_{kn} - \delta_{jn} \delta_{km}} (F_{m;k} G_n + F_m G_{n;k})$$

$$= \hat{e}_j (F_{j,k} G_k - F_{k,j} G_j + F_j G_{k,j} - F_k G_{j,k})$$

$$\nabla \times (\vec{F} \times \vec{G}) = (\vec{G} \cdot \nabla) \vec{F} - (\vec{F} \cdot \nabla) \vec{G} + \vec{F} \nabla \cdot \vec{G} - \vec{G} \nabla \cdot \vec{F}$$

this set of symbols means  $G_k \nabla_k (F_j \hat{e}_j) = \hat{e}_j G_k F_{j,k}$

$$\textcircled{2} \nabla (\vec{F} \cdot \vec{G}) = \hat{e}_j (F_k G_{k,j})_j$$

$$= \hat{e}_j \underbrace{F_{k,j} G_k + \hat{e}_j F_k G_{k,j}}_j$$

$$= \hat{e}_j (F_{k,j} - F_{j,k} + F_{j,k}) G_k$$

Use

$$= \hat{e}_j (F_{k,j} - F_{j,k}) G_k + \hat{e}_j G_k F_{j,k}$$

$$\epsilon_{ijk} \epsilon_{lmn} F_{lm} = (\delta_{jm} \delta_{kn} - \delta_{jn} \delta_{km}) F_{lm} \rightarrow = \hat{e}_j \epsilon_{ijk} \epsilon_{lmn} F_{lm} G_k + \hat{e}_j G_k F_{j,k}$$

$$= F_{k,j} - F_{j,k}$$

$$= \hat{e}_j \epsilon_{jkl} G_k \epsilon_{lmn} F_{lm} + \hat{e}_j G_k F_{j,k}$$

$$\text{So } \nabla (\vec{F} \cdot \vec{G}) = \vec{G} \times (\nabla \times \vec{F}) + \vec{F} \times (\nabla \times \vec{G}) + (\vec{G} \cdot \nabla) \vec{F} + (\vec{F} \cdot \nabla) \vec{G}$$