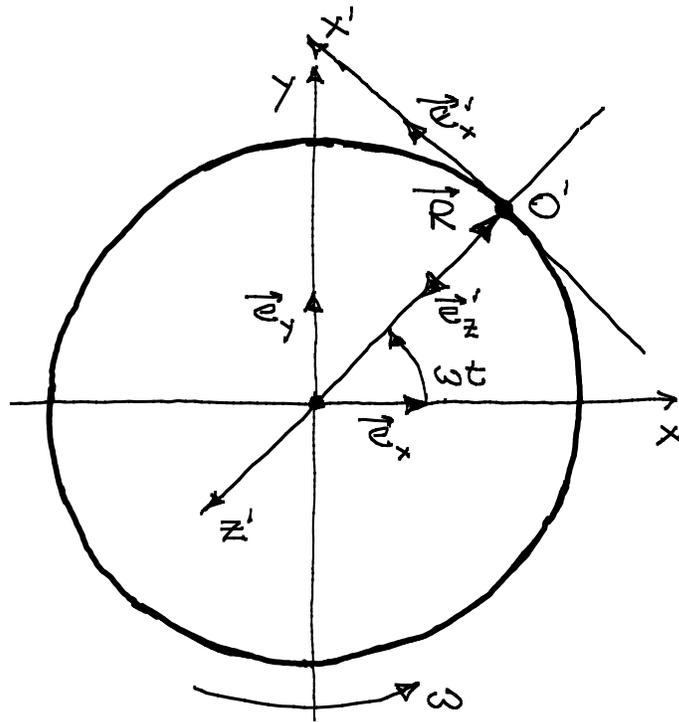


Phys 503
Midterm # 2
Solution Set



$\vec{\omega}_z$ out of page
 $\vec{\omega}_z^-$ into page

We will need

$$\vec{e}_x' = -\vec{e}_x \sin \omega t + \vec{e}_y \cos \omega t$$

$$\vec{e}_y' = -\vec{e}_y \sin \omega t - \vec{e}_x \cos \omega t$$

$$\vec{e}_z' = \vec{e}_z$$

and $x' = -x \sin \omega t + y \cos \omega t$

$$y' = -x \cos \omega t - y \sin \omega t$$

$$z' = z$$

$$\vec{e}_i' = A_{jk} \vec{e}_j \quad A = \begin{pmatrix} -\sin & \cos & 0 \\ \cos & \sin & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$x_i' \vec{e}_i' = R + x_j' \vec{e}_j' = (x_j' - R \delta_{ij}') \vec{e}_i' = (x_j' - R \delta_{ij}') A_{ik} \vec{e}_k$$

$$\rightarrow x_k = (x_i' - R \delta_{ij}') A_{ik}$$

$$\text{or } (x \ y \ z) = (x' \ y' \ z' - R) A$$

$$\text{or } (x \ y \ z' - R) = (x' \ y' \ z') A^T$$

$$\begin{pmatrix} x \\ y \\ z' - R \end{pmatrix} = A \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}$$

(2)

$$\dot{\vec{e}}_z' = \omega \vec{e}_z' = -\omega \vec{e}_z'$$

$$\dot{\vec{e}}_x' = -\omega \vec{e}_y' = \omega (\cos \omega t \vec{e}_x + \sin \omega t \vec{e}_y)$$

$$\dot{\vec{e}}_y' = \omega \vec{e}_x' = \omega (-\sin \omega t \vec{e}_x + \cos \omega t \vec{e}_y) = \omega_x \dot{\vec{e}}_x' = \omega \dot{\vec{e}}_x'$$

$$\dot{\vec{e}}_z' = \omega^p \dot{\vec{e}}_z' = \omega^p \vec{e}_z' = \omega^p \dot{\vec{e}}_z'$$

(b) Method 1: Use the equations for a rotating frame

(10)

$$\vec{a}'_r = \underbrace{-\omega \times (\omega \times \vec{r})}_{\text{main centrifugal acceleration}} - \omega \times (\omega \times \vec{r}) - \underbrace{2\omega \times \vec{v}'_r}_{\text{Coriolis force}}$$

$$- \omega^2 \vec{r} = -\omega^2 x'_i \vec{e}'_x - \omega^2 z'_i \vec{e}'_z$$

$$- \omega^2 \vec{e}'_y \times (\vec{e}'_y \times \vec{r}) = -\omega^2 \vec{e}'_y \times (-x'_i \vec{e}'_z + z'_i \vec{e}'_x)$$

$$= \omega^2 x'_i \vec{e}'_x + \omega^2 z'_i \vec{e}'_z$$

additional centrifugal acceleration when not at O'_i

$$\begin{aligned} \ddot{x}'_i &= \omega^2 x'_i + 2\omega \dot{z}'_i \\ \ddot{z}'_i &= -\omega^2 (R - z'_i) - 2\omega \dot{x}'_i \\ \ddot{y}'_i &= 0 \end{aligned}$$

Method 2. Write the primed coordinates in terms of the inertial coordinates.

$$x'_i = -x \sin \omega t + y \cos \omega t$$

$$y'_i = -z$$

$$z'_i = R - x \cos \omega t - y \sin \omega t$$

The inertial coordinates satisfy

$$\ddot{x} = \ddot{y} = \ddot{z} = 0,$$

so

$$\ddot{x}'_i = -\ddot{x} \cos \omega t + \ddot{y} \sin \omega t - \omega^2 (x \cos \omega t + y \sin \omega t)$$

$$\ddot{x}'_i = -\omega^2 (x \cos \omega t + y \sin \omega t) + \omega^2 (x \cos \omega t - y \sin \omega t)$$

$$= -\omega^2 x'_i - \omega^2 z'_i$$

$$\ddot{z}'_i = -\ddot{z} \cos \omega t - \ddot{x} \sin \omega t + \omega^2 (x \sin \omega t - y \cos \omega t)$$

$$\ddot{z}'_i = \omega^2 (x \sin \omega t - y \cos \omega t) + \omega^2 (x \cos \omega t + y \sin \omega t)$$

$$= \omega^2 (R - z'_i) - \omega^2 x'_i$$

$$\begin{aligned} \ddot{x}'_i &= \omega^2 x'_i + 2\omega \dot{z}'_i \\ \ddot{z}'_i &= -\omega^2 (R - z'_i) - 2\omega \dot{x}'_i \\ \ddot{y}'_i &= 0 \end{aligned}$$

(c) Initial conditions: $x'(0)=0, \dot{x}'(0)=0, z'(0)=h, \dot{z}'(0)=0$

Method 1. One neglects the tiny centrifugal corrections $\omega^2 x'$ and $\omega^2 z'$. In addition, one neglects the Coriolis term in the z' equation. So

$$\ddot{z}' = -\omega^2 R \Rightarrow \dot{z}' = -\omega^2 R t \text{ and } z' = h - \frac{1}{2} \omega^2 R t^2$$

fall under effective gravity $g = \omega^2 R$

$$\ddot{x}' = 2\omega \dot{z}' = -2\omega^2 R t \Rightarrow x' = -\frac{1}{3} R (\omega t)^3$$

$$\begin{aligned} z'(t) &= h - \frac{1}{2} R (\omega t)^2 \\ x' &= -\frac{1}{3} R (\omega t)^3 \end{aligned}$$

Method 2. One can easily find the exact solution in the inertial coordinates.

Initial conditions: $x(0) = R-h, \dot{x}(0)=0, y(0)=0, \dot{y}(0) = \omega(R-h)$

$$\Rightarrow x(t) = R-h \text{ and } y(t) = \omega t (R-h)$$

Exact: $x'(t) = (R-h) (-\sin \omega t + \omega t \cos \omega t)$

$$\omega t \ll 1: -\omega t + \frac{1}{6} (\omega t)^3 + \omega t - \frac{1}{6} (\omega t)^3 = -\frac{1}{6} (\omega t)^3$$

Exact: $z'(t) = R - (R-h) (\cos \omega t + \omega t \sin \omega t)$

$$\omega t \ll 1: 1 - \frac{1}{2} (\omega t)^2 + (\omega t)^2 = 1 + \frac{1}{2} (\omega t)^2$$

$$\omega t \ll 1: z' = h - \frac{1}{2} (R-h) (\omega t)^2 = h - \frac{1}{2} R (\omega t)^2$$

neglect

$$x' = -\frac{1}{3} (R-h) (\omega t)^3 = -\frac{1}{3} R (\omega t)^3$$

$$\begin{aligned} z'(t) &= h - \frac{1}{2} R (\omega t)^2 \\ x' &= -\frac{1}{3} R (\omega t)^3 \end{aligned}$$

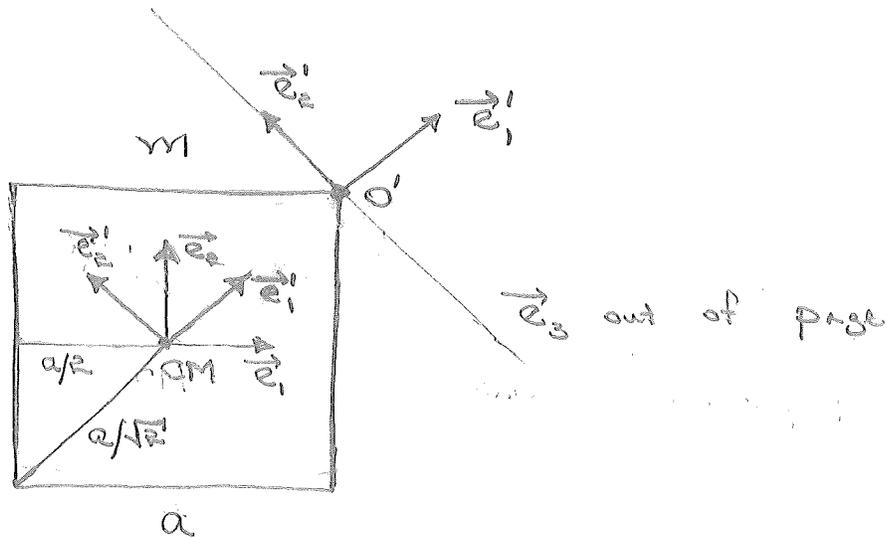
The particle hits the ground at $t = \sqrt{2h/g}$, $g = 5^2 \text{ m/s}^2$,
When

$$x = \frac{1}{2} g t^2 = \frac{1}{2} \times 5^2 \times \left(\frac{\sqrt{2h}}{5} \right)^2 = \frac{1}{2} \times 2h = h$$

so

$$\frac{x}{h} = \frac{\frac{1}{2} g t^2}{h} = \frac{\frac{1}{2} \times 5^2 \times \frac{2h}{5^2}}{h} = 1$$

x would be about 20 cm, so you could see this is a careful measurement.



Surface density $\sigma = m/a^2$

(a) Inertia tensor about CM: $\vec{I}_{CM} = \int \sigma dA (\vec{r}^2 \vec{I} - \vec{r} \otimes \vec{r})$

Principal axes: $\vec{e}_1, \vec{e}_2, \vec{e}_3$ shows

$$I_{13} = - \int \sigma dA xz = 0$$

$$I_{23} = - \int \sigma dA yz = 0 \quad \begin{array}{l} \updownarrow \\ \text{because square is thin} \\ (z=0) \end{array}$$

$$I_{12} = - \int \sigma dA xy = 0$$

↑ because of reflection symmetry $x \rightarrow -x$ or $y \rightarrow -y$.

$$I_{11} = \int \sigma dA (y^2 + z^2) = \int \sigma dA y^2 =$$

$$= \frac{m}{a^2} \int_{-a/2}^{+a/2} dx \int_{-a/2}^{+a/2} y^2 dy$$

$$= \frac{1}{2} \frac{1}{3} \left(\frac{a}{2}\right)^3 = \frac{1}{12} a^3$$

$$\boxed{I_{11} = \frac{1}{12} m a^2}$$

$$I_{zz} = \int \sigma dA (x^2 + z^2) = \int \sigma dA x^2 = I_{xx}$$

$$I_{zz} = \frac{1}{12} ma^2$$

$$I_{yy} = \int \sigma dA (x^2 + y^2) = I_{xx} + I_{zz} = \frac{1}{6} ma^2 = I_{yy}$$

Since $I_{xx} = I_{zz}$, any pair of orthogonal vectors in the plane of the square are principal axes.

In particular, \vec{e}'_1 and \vec{e}'_2 are principal axes with $I'_{xx} = I'_{zz} = \frac{1}{12} ma^2$.

(b) Inertia tensor about O' : $\vec{I}_{O'} = \int \sigma dA (x'^2 \vec{1} - \vec{r}' \otimes \vec{r}')$

Principal axes: $\vec{e}'_1, \vec{e}'_2, \vec{e}'_3$ shown

These axes are unique because the 3 principal moments of inertia are different

Use $\vec{I}_{O'} = \vec{I}_{CM} + m(\vec{R} \vec{1} - \vec{R} \otimes \vec{R})$

$\vec{R} = \frac{1}{\sqrt{2}} \vec{e}'_1$ is the vector from O' to CM.

$$\therefore \vec{I}_{O'} = \vec{I}_{CM} + \frac{1}{12} ma^2 (\vec{1} - \underbrace{\vec{e}'_1 \otimes \vec{e}'_1}_{\vec{e}'_2 \otimes \vec{e}'_2 + \vec{e}'_3 \otimes \vec{e}'_3})$$

This shows \vec{e}'_1, \vec{e}'_2 , and \vec{e}'_3 are principal axes

$$\begin{aligned} (I_{O'})'_{xx} &= I'_{xx} = \frac{1}{12} ma^2 \\ (I_{O'})'_{yy} &= I'_{yy} + \frac{1}{12} ma^2 = \frac{7}{12} ma^2 \\ (I_{O'})'_{zz} &= I'_{zz} + \frac{1}{12} ma^2 = \frac{1}{12} ma^2 \end{aligned}$$



Method 1

$$T = T_{CM} + T_{rot \text{ about CM}}$$

$$T_{CM} = \frac{1}{2} m \left(\frac{a}{\sqrt{2}} \dot{\theta} \right)^2 = \frac{1}{4} m a^2 \dot{\theta}^2$$

$$T_{rot \text{ about CM}} = \frac{1}{2} I'_{CM} \dot{\theta}^2 = \frac{1}{24} m a^2 \dot{\theta}^2$$

$$T = \frac{7}{24} m a^2 \dot{\theta}^2$$

$$T = \frac{7}{24} m a^2 \dot{\theta}^2 = T$$

Method 2: $T = T_{rot \text{ about } O'} = \frac{1}{2} (I_{O'})' \dot{\theta}^2 = \frac{7}{24} m a^2 \dot{\theta}^2 = T$

$$V = mg \left(-\frac{a}{\sqrt{2}} \cos \theta \right) = -\frac{1}{\sqrt{2}} m g a \cos \theta = V$$

$$L = T - V = \frac{7}{24} m a^2 \dot{\theta}^2 + \frac{1}{\sqrt{2}} m g a \cos \theta = L$$

Small oscillations:

$$L = \frac{7}{24} m a^2 \dot{\theta}^2 - \frac{1}{\sqrt{2}} m g a \theta^2 + \frac{1}{\sqrt{2}} m g a$$

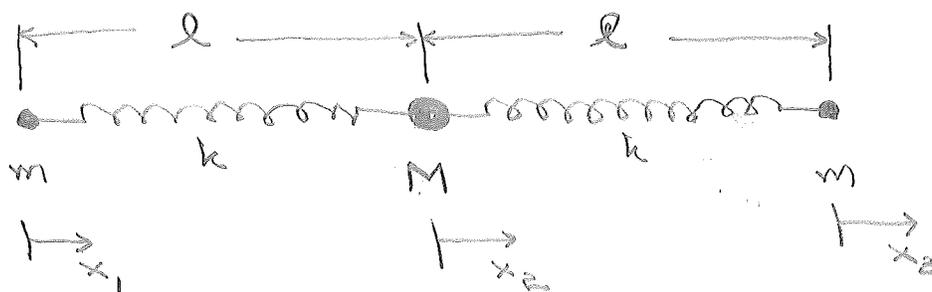
$$\cos \theta \approx 1 - \frac{1}{2} \theta^2$$

$$= \frac{7}{24} m a^2 \left(\dot{\theta}^2 - \frac{12}{\sqrt{2}} \frac{g}{a} \theta^2 \right) + \frac{1}{\sqrt{2}} m g a$$

$$\omega = \sqrt{\frac{12}{\sqrt{2}}} \sqrt{\frac{g}{a}}$$

3. Linear triatomic molecule

Exam: specialize to $M = 2m$



$$(a) \quad T = \frac{1}{2} m (\dot{x}_1^2 + \dot{x}_3^2) + \frac{1}{2} M \dot{x}_2^2$$

$$= \frac{1}{2} (\dot{x}_1 \quad \dot{x}_2 \quad \dot{x}_3) \begin{pmatrix} m & 0 & 0 \\ 0 & M & 0 \\ 0 & 0 & m \end{pmatrix} \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix}$$

$$V = \frac{1}{2} k \left[\overbrace{(x_2 - x_1)^2}^{(x_2 + l - x_1 - l)^2} + \overbrace{(x_3 - x_2)^2}^{(x_3 + l - x_2 - l)^2} \right]$$

$$x_1^2 + 2x_2^2 + x_3^2 - 2x_1x_2 - 2x_2x_3$$

$$= \frac{1}{2} (x_1 \quad x_2 \quad x_3) k \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$

✓

$$T = m \underbrace{\begin{pmatrix} 1 & 0 & 0 \\ 0 & M/m & 0 \\ 0 & 0 & 1 \end{pmatrix}}_t = mt$$

$$V = k \underbrace{\begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix}}_v = kv$$

(b-e) Eigenvalue problem: $Q = (V - \omega^2 T) a = k \left(v - \frac{\omega^2}{k/m} t \right)$
 $= \underbrace{\left\{ \begin{matrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{matrix} \right\}}_v - \underbrace{\left\{ \begin{matrix} 1 & 0 & 0 \\ 0 & M/m & 0 \\ 0 & 0 & 1 \end{matrix} \right\}}_t$

$$(v - \omega^2 t) a = 0, \quad \omega^2 = \frac{\omega^2}{k/m}$$

Guess method: There are two obvious normal modes: (i) all masses in uniform motion, with no restoring forces,

$$a_1 = \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}, \Rightarrow \omega_1 = 0$$

$$v a_1 = \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

$\omega_1^2 = 0$

(ii) middle mass at rest, outer two masses out of phase

$$Q_{p1} = \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix} \quad 2$$

$$\omega_p = \sqrt{k/m}$$

$$vR_2 = \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix} \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}$$

$$tR_2 = \begin{pmatrix} 1 & 0 & 0 \\ 0 & M/m & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}$$

$$vR_2 = tR_2 \Rightarrow d_2 = 1$$

The third mode must be orthogonal to Q_1 and Q_2 relative to t :

$$Q_3 = \begin{pmatrix} Q_{13} \\ Q_{23} \\ Q_{33} \end{pmatrix}$$

$$0 = Q_1^T t R_3 = \begin{pmatrix} 1 & 1 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & M/m & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} Q_{13} \\ Q_{23} \\ Q_{33} \end{pmatrix}$$

$$= Q_{13} + \frac{M}{m} Q_{23} + Q_{33}$$

$$0 = Q_2^T t R_3 = \begin{pmatrix} 1 & 0 & -1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & M/m & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} Q_{13} \\ Q_{23} \\ Q_{33} \end{pmatrix}$$

$$= Q_{13} - Q_{33}$$

$\Rightarrow Q_{13} = Q_{33} = 1$ } choose

$$Q_{23} = -\frac{M}{m} Q_{13} = -\frac{M}{m}$$

$$a_3 = \begin{pmatrix} 1 \\ -2m/M \\ 1 \end{pmatrix}$$

$$\text{Check: } v a_3 = \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix} \begin{pmatrix} 1 \\ -2m/M \\ 1 \end{pmatrix} = \begin{pmatrix} 1 + 2m/M \\ -2 - 4m/M \\ 1 + 2m/M \end{pmatrix} = \left(1 + \frac{2m}{M}\right) \begin{pmatrix} 1 \\ -2 \\ 1 \end{pmatrix}$$

$$t a_3 = \begin{pmatrix} 1 & 0 & 0 \\ 0 & M/m & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 \\ -2m/M \\ 1 \end{pmatrix} = \begin{pmatrix} 1 \\ -2 \\ 1 \end{pmatrix}$$

$$\Rightarrow v a_3 = \underbrace{\left(1 + \frac{2m}{M}\right)}_{\alpha_3^2} t a_3$$

$$a_3 = \begin{pmatrix} 1 \\ -2m/M \\ 1 \end{pmatrix}, \quad \omega_3 = \sqrt{1 + 2m/M} \sqrt{k/m}$$

Official method:

$$(v - \alpha^2 t) a = 0$$

$$\begin{aligned} \text{Secular equation: } 0 &= \det(v - \alpha^2 t) \\ &= \det \begin{pmatrix} 1 - \alpha^2 & -1 & 0 \\ -1 & 2 - \alpha^2 M/m & -1 \\ 0 & -1 & 1 - \alpha^2 \end{pmatrix} \\ &= (1 - \alpha^2) \left((2 - \alpha^2 \frac{M}{m})(1 - \alpha^2) - 1 \right) \\ &\quad - (1 - \alpha^2)^2 \end{aligned}$$

$$0 = (1 - \alpha^2) \left(\sqrt{\frac{p}{3}} - \alpha^2 \frac{p}{3} - 2\alpha^2 + \alpha^4 \frac{p}{3} - 1 + 1 \right)$$

$$= (1 - \alpha^2) \alpha^2 \left(\frac{p}{3} \alpha^2 - \left(2 + \frac{p}{3} \right) \right)$$

$$0 = (1 - \alpha^2) \alpha^2 \left(\alpha^2 - \left(1 + \frac{p}{3} \right) \right)$$

$$\rightarrow \alpha_1^p = 0, \quad \alpha_2^p = 1, \quad \alpha_3^p = 1 + \frac{p}{3}$$

$$\omega_1 = 0, \quad \omega_2 = \sqrt{km}, \quad \omega_3 = \sqrt{1 + 2m/M} \sqrt{km}$$

Mode 1: $0 = (U - t) R_1 = \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & -1 \end{pmatrix} \begin{pmatrix} R_{11} \\ R_{21} \\ R_{31} \end{pmatrix}$

$$\begin{aligned} 0 &= R_{11} - R_{21} \\ 0 &= R_{21} - R_{31} \end{aligned} \Rightarrow R_{31} = R_{21} = R_{11}$$

$$R_1 \propto \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

Mode 2: $0 = (U - t) R_2 = \begin{pmatrix} 0 & -1 & 0 \\ -1 & 2 - \frac{p}{3} & -1 \\ 0 & -1 & 0 \end{pmatrix} \begin{pmatrix} R_{12} \\ R_{22} \\ R_{32} \end{pmatrix}$

$$\Rightarrow R_{22} = 0, \quad -R_{12} - R_{32} = 0 \Rightarrow R_{32} = -R_{12}$$

$$R_2 \propto \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}$$

Mode 3:

$$0 = \left(v - \left(1 + \frac{2m}{M} \right) t \right) \mathbf{a}_3 = \begin{pmatrix} 2m/M & -1 & 0 \\ -1 & -M/m & -1 \\ 0 & -1 & 2m/M \end{pmatrix} \begin{pmatrix} a_{13} \\ a_{23} \\ a_{33} \end{pmatrix} \quad (1)$$

$$0 = \frac{2m}{M} a_{13} - a_{23} = \frac{2m}{M} a_{33} - a_{23} \Rightarrow a_{13} = a_{33}$$

$$0 = -a_{13} - a_{23} - \frac{1}{3} a_{23} = -a_{13} - \frac{4}{3} a_{23}$$

$$\Rightarrow a_{23} = -\frac{3}{4} a_{13}$$

$$\mathbf{a}_3 \propto \begin{pmatrix} 1 \\ -2m/M \\ -1 \end{pmatrix}$$