

Physics 406: P.S#4 Solutions

(Griffiths 7.16)

The previous problem gave the solution in the "quasi-static" regime. That is to say, we calculated \vec{B} from Ampère's Law excluding any displacement-current, and then used this to find the induced \vec{E} via Faraday's Law.

This will be valid as long as

$$L \ll cT$$

where L is any characteristic dimension of interest and T is the characteristic time in which currents are changing, c is the speed of light.

Now let's find the missing displacement-current.

In the geometry of the problem



$$\vec{E}(r, t) = \frac{\mu_0 I}{2\pi} \cos \omega t \ln\left(\frac{R}{r}\right) \hat{z}$$

7.33 (a) The displacement current density

$$\vec{J}_d = \epsilon_0 \frac{\partial \vec{E}}{\partial t} = \left[\frac{\epsilon_0 I}{2\pi} \frac{\omega^2}{c^2} \cos \omega t \ln\left(\frac{R}{r}\right) \hat{z} \right]$$

(Having used $c = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$)

7.33(b) The total displacement current is the flux of \vec{J}_d through the area enclosed by the cylinder

$$I_d = \int \vec{J}_d \cdot d\vec{a} = \int_0^R \vec{J}_d \cdot (2\pi r dr \hat{z})$$

$$= I \frac{\omega^2}{c^2} \cos \omega t \int_0^R r \ln\left(\frac{r}{R}\right) dr$$

Aside: $r \ln\left(\frac{R}{r}\right) = \frac{1}{2} \frac{d(r^2)}{dr} \ln\left(\frac{R}{r}\right) = \frac{1}{2} \left(\frac{d}{dr} (r^2 \ln\left(\frac{R}{r}\right)) - r^2 \frac{d}{dr} \ln\left(\frac{R}{r}\right) \right)$

(Integration by parts) $= \frac{1}{2} \left(\frac{d}{dr} (r^2 \ln\left(\frac{R}{r}\right)) + r \right)$

$$\therefore \int_0^R r \ln\left(\frac{r}{R}\right) dr = \left[\frac{r^2}{2} \ln\left(\frac{R}{r}\right) + \frac{r^2}{4} \right]_0^R = \frac{R^2}{4} \quad \left(\begin{array}{l} \text{since } \ln \\ \text{diverges} \\ \text{slower than } r^2 \end{array} \right)$$

$$\therefore \boxed{I_d = \frac{1}{4} \frac{\omega^2 R^2}{c^2} I \cos \omega t}$$

7.33(c) $\frac{I_d(t)}{I \cos \omega t} = \frac{1}{4} \frac{\omega^2 R^2}{c^2}$, Given $R = 2 \text{ mm} = 2 \times 10^{-3} \text{ m}$

$$\frac{I_d}{I \cos \omega t} = 0.1 = \frac{1}{4} \frac{\omega^2 R^2}{c^2}$$

$$\Rightarrow \omega^2 = 0.4 \frac{c^2}{R^2}$$

$$\omega = \sqrt{0.4} \frac{c}{R} = 9.5 \times 10^{10} \text{ rad/sec}$$

$$\nu = \frac{\omega}{2\pi} = 15 \text{ GHz}$$

A pretty big (but not unreasonable frequency)

(Next page)

Comments.

We see here that $\frac{I_d}{I_{\text{conduction}}} \sim \frac{\omega^2 R^2}{c^2} \sim \left(\frac{R}{cT}\right)^2 \ll 1$

As expected, the displacement current is negligible if the time it takes light to propagate across the dimension of the system is small compare to the ~~period~~ time over which the current changes

$$\frac{R}{c} \ll T \quad (\text{Quasi static})$$

Stated another way, we know that

$$\frac{\omega}{c} = k = \frac{2\pi}{\lambda}, \quad \text{where } \lambda \text{ is the wavelength of the wave created by a signal oscillating at } \omega$$

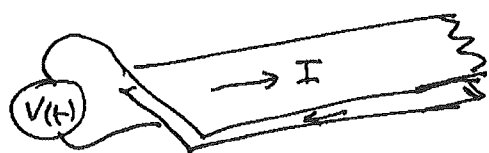
$$\text{Thus } \frac{\omega^2 R^2}{c^2} \sim \frac{R^2}{\lambda^2} \ll 1$$

$$R \ll \lambda \quad (\text{Quasi static})$$

Of course, this is all a bit of a fudge since we assumed an infinitely long cylinder. This will only be self consistent if

$$L \ll \lambda \quad \text{i.e.} \quad \frac{L}{c} \ll T$$

Problem 2: Parallel Plate Transmission Line



The problem here is to show how voltage and current propagate down a "transmission line".

Our first task is to determine the capacitance and inductance / length.

Let's give the line dimensions



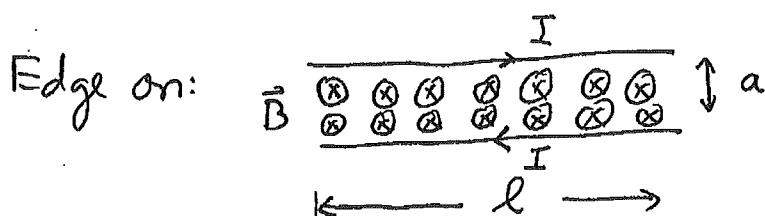
The capacitance of parallel plates

$$C = \epsilon_0 \frac{A}{a} = \epsilon_0 \frac{bl}{a}$$

$$\Rightarrow \frac{\text{Capacitance}}{\text{length}} \quad \mathcal{C} = \frac{C}{l} = \boxed{\epsilon_0 \frac{b}{a}}$$

To find inductance, we put current on the plates, and determine the flux through a surface. Then

$$\Phi = LI$$



$$\Rightarrow \Phi = B a l$$

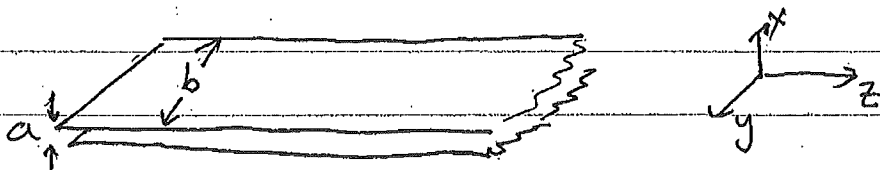
$$B = \mu_0 K \quad \text{for parallel plates} \\ \text{(see 405)}$$

$$K = \frac{I}{b}$$

$$\Rightarrow \Phi = \mu_0 \frac{a l}{b} I \quad \Rightarrow \quad L = \mu_0 \frac{a l}{b}$$

$$\Rightarrow \boxed{\mathcal{L} = \frac{L}{l} = \mu_0 \frac{a}{b}}$$

Transmission Line



(a) Maxwell's equations: Between the plates $\rho = \vec{J} = 0$

We also know $\vec{E}(\vec{r}, t) = E_x(z, t) \hat{x}$
 $\vec{B}(\vec{r}, t) = B_y(z, t) \hat{y}$

$$\Rightarrow \frac{\partial E_x}{\partial x} = 0, \quad \frac{\partial B_y}{\partial y} = 0, \quad \frac{\partial E_x}{\partial z} = -\frac{\partial B_y}{\partial t}, \quad \frac{\partial B_y}{\partial z} = -\mu_0 \epsilon_0 \frac{\partial E_x}{\partial t}$$

\uparrow Gauss \uparrow no mag. monopoles \uparrow Faraday \uparrow Ampère

Now, the electric and magnetic fields are related to the local voltage and current

$$V = + \int_0^a E_x dx \Rightarrow E_x = \frac{V}{a}$$

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} \Rightarrow B_y = \mu_0 \frac{I}{b}$$

\leftarrow surface current

Faraday's Law $\Rightarrow \frac{\partial}{\partial z} \left(\frac{V}{a} \right) = -\frac{\partial}{\partial t} \left(\frac{\mu_0 I}{b} \right)$

$$\Rightarrow \boxed{\frac{\partial V}{\partial z} = -\frac{\mu_0 a}{b} \frac{\partial I}{\partial t} = -L \frac{\partial I}{\partial t}}$$

$$\Rightarrow \frac{\partial}{\partial z} \left(\frac{\mu_0 I}{b} \right) = -\mu_0 \epsilon_0 \frac{\partial}{\partial t} \left(\frac{V}{a} \right)$$

$$\Rightarrow \boxed{\frac{\partial I}{\partial z} = -\frac{\epsilon_0 b}{a} \frac{\partial V}{\partial t} = -C \frac{\partial V}{\partial t}}$$

(b) We want to derive the wave equation from the coupled set of first order P.D.E.s

- Take $\frac{\partial}{\partial z}$ of Faraday's Law

$$\frac{\partial}{\partial z} \left(\frac{\partial V}{\partial z} \right) = - \frac{\partial}{\partial z} \left(L \frac{\partial I}{\partial t} \right)$$

↓

$$\frac{\partial^2 V}{\partial z^2} = - L \frac{\partial}{\partial t} \left(\frac{\partial I}{\partial z} \right)$$

[Having switched the order of derivatives]

↓

$$\boxed{\frac{\partial^2 V}{\partial z^2} = + LC \frac{\partial^2 V}{\partial t^2}}$$

[Substituting for $\frac{\partial I}{\partial z}$ from Ampère's Law]

- Similarly, take $\frac{\partial}{\partial z}$ of Ampère's Law

$$\frac{\partial}{\partial z} \left(\frac{\partial I}{\partial z} \right) = - \frac{\partial}{\partial z} \left(C \frac{\partial V}{\partial t} \right)$$

↓

$$\frac{\partial^2 I}{\partial z^2} = - C \frac{\partial}{\partial t} \left(\frac{\partial V}{\partial z} \right)$$

↓

$$\boxed{\frac{\partial^2 I}{\partial z^2} = LC \frac{\partial^2 I}{\partial t^2}}$$

Thus the local voltage and current satisfy the wave equation

$$\left(\frac{\partial^2}{\partial z^2} - \frac{1}{v^2} \frac{\partial^2}{\partial t^2} \right) f = 0$$

(Next Page)

Comparing the wave eq. for V and I with the general form, we find the phase velocity

$$v = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{\left(\frac{\mu_0 a}{b}\right)\left(\frac{\epsilon_0 b}{a}\right)}} = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = c!$$

Thus the voltage and current waves propagate at the speed of light!

(c) Let's plug in the trial solutions

$$V(z,t) = V_0 \cos(kz - \omega t) \quad I(z,t) = I_0 \cos(kz - \omega t)$$

$$\frac{\partial^2 V}{\partial z^2} = -k^2 V$$

$$\frac{\partial^2 V}{\partial t^2} = -\omega^2 V$$

$$\Rightarrow -k^2 + \frac{\omega^2}{LC} = 0$$

Thus our ansatz is a solution iff

$$\frac{\omega}{k} = \frac{1}{\sqrt{LC}} = c \quad \text{the phase velocity}$$

The same is true for the current wave

(Next page)

Now, the amplitude of the voltage and current waves are not independent. They are coupled by Maxwell's eqns:

$$\frac{\partial I}{\partial z} = -\epsilon \frac{\partial V}{\partial t} \Rightarrow -k I_0 \sin(kz - \omega t) = -\omega \epsilon V_0 \times \sin(kz - \omega t)$$

$$\Rightarrow V_0 = \frac{k}{\omega \epsilon} I_0$$

But $\frac{\omega}{k} = \frac{1}{\sqrt{\epsilon \mu}}$ \Rightarrow $V_0 = \sqrt{\frac{\mu}{\epsilon}} I_0$

Thus the voltage and current amplitudes satisfies an "Ohm's Law" with the proportionality constant known as the "characteristic impedance" of the line

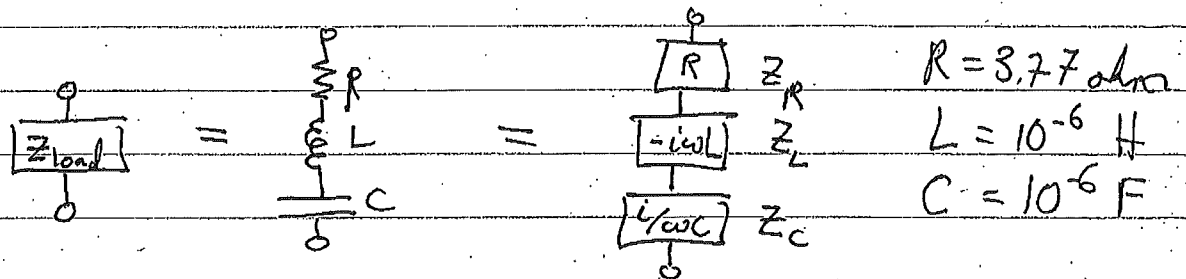
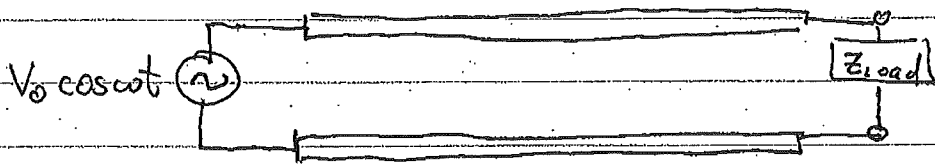
$$Z_c = \sqrt{\frac{\mu}{\epsilon}} = \sqrt{\frac{\mu_0 a}{\epsilon_0 b}} = \sqrt{\frac{\mu_0}{\epsilon_0}} \frac{a}{b}$$

$$\Rightarrow Z_c = Z_0 \frac{a}{b}$$

where $Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = \sqrt{\frac{4\pi \times 10^{-7} \text{ N/A}^2}{8.85 \times 10^{-12} \frac{\text{coul}}{\text{Volt} \cdot \text{m}}}} = 377 \text{ ohms}$

This is known as the impedance of free space

(d) Now a load terminates the transmission line



$$Z_{load} = R - i\omega L + \frac{i}{\omega C}$$

$$= R \left(1 - i \frac{1}{\omega} (\omega^2 - \omega_0^2) \right)$$

$$\Gamma = \frac{L}{R} \text{ (damping)} \quad \omega_0 = \frac{1}{\sqrt{LC}} \text{ (resonance frequency)}$$

The characteristic impedance of the transmission line for the case $b = 100a$...

$$Z_c = \frac{a}{b} Z_0 = \frac{1}{100} Z_0 = 3.77 \text{ ohm}$$

⇒ The load impedance will match the characteristic impedance if

$$\omega = \omega_0 = \frac{1}{\sqrt{LC}} = 10^6 \text{ s}^{-1}$$

resonance

Problem 3

$$\text{Given } \vec{E}(\vec{r}, t) = (\hat{x} + 2\hat{y} + E_z \hat{z}) \cos(-3x + y + z - \omega t)$$

The general form of a plane wave (linearly polarized)

$$\vec{E}(\vec{r}, t) = \vec{E}_0 \cos(\vec{k} \cdot \vec{r} - \omega t + \phi)$$

$$\vec{k} \cdot \vec{r} = -3x + y + z \Rightarrow \vec{k} = -3\hat{x} + \hat{y} + \hat{z}$$

$$\vec{E}_0 = \hat{x} + 2\hat{y} + E_z \hat{z}$$

(a) Direction of propagation $\hat{k} = \frac{\vec{k}}{|\vec{k}|}$, $|\vec{k}| = \frac{\sqrt{3^2 + 1^2 + 1^2}}{\sqrt{11}}$

$$\therefore \hat{k} = \frac{1}{\sqrt{11}}(-3\hat{x} + \hat{y} + \hat{z})$$

(b) $\vec{\nabla} \cdot \vec{E} = 0 \Rightarrow \vec{k} \cdot \vec{E}_0 = 0 = (-3\hat{x} + \hat{y} + \hat{z}) \cdot (\hat{x} + 2\hat{y} + E_z \hat{z})$

$$\therefore -3 + 2 + E_z = 0 \Rightarrow E_z = 1 \frac{\text{Volt}}{\text{m}}$$

Polarization is linear, along direction

$$\vec{E} = \frac{\vec{E}_0}{|\vec{E}_0|} = \frac{1}{\sqrt{6}}(\hat{x} + 2\hat{y} - \hat{z})$$

(c) Wavelength: $\lambda = \frac{2\pi}{|\vec{k}|} = \frac{2\pi}{\sqrt{11}} \text{ m}$

(d) Frequency $\nu = \frac{\omega}{2\pi} = \frac{c k}{2\pi} = \frac{c}{\lambda}$

$$\Rightarrow \nu = \frac{3 \times 10^8 \text{ m/s}}{\frac{2\pi}{\sqrt{11}} \text{ m}} = 1.6 \times 10^8 \text{ s}^{-1} = 160 \text{ MHz}$$

(TV broadcast)

(Next Page)

Problem 3 continued

(c) For a travelling plane wave, the magnetic field generally has the same form as the electric field.

$$\vec{B} = \vec{B}_0 \cos(\vec{k} \cdot \vec{r} - \omega t + \phi) \quad (\text{in phase with electric field})$$

with $\vec{k} \cdot \vec{B}_0 = 0$, $\vec{E}_0 \cdot \vec{B}_0 = 0$, $\vec{E}_0 \times \vec{B}_0 \propto \vec{k}$

$$\text{and } B_0 = E_0 / c$$

If the wave were propagating along one of the Cartesian axes, we could use those to simply write down the magnetic field. For this more complicated geometry it is easier to return directly to Maxwell's eqn.

Use complex representation: $\vec{E} = \vec{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$
 $\vec{B} = \vec{B}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \Rightarrow i\vec{k} \times \vec{E}_0 = i\omega \vec{B}_0 \quad \left(\begin{array}{l} \vec{\nabla} \rightarrow +i\vec{k} \\ \frac{\partial}{\partial t} \rightarrow -i\omega \end{array} \right) \quad (\text{Remember})$$

$$\Rightarrow \vec{B}_0 = \frac{\vec{k} \times \vec{E}_0}{\omega} = \frac{\vec{k}}{ck} \times \vec{E}_0$$

$$= \frac{1}{ck} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ -3 & 1 & 1 \\ 1 & 2 & 1 \end{vmatrix} = \frac{1}{ck} [-\hat{x} + 4\hat{y} - 7\hat{z}]$$

$$ck = \omega = 2\pi\nu = 3\sqrt{11} \times 10^8 \text{ s}^{-1}$$

$$\Rightarrow \boxed{\vec{B}(\vec{r}, t) = \frac{10^{-8}}{3\sqrt{11}} (-\hat{x} + 4\hat{y} - 7\hat{z}) \cos(-3x + y + z - \omega t)}$$